



# The Real FT8, JT65, and JT9 Signal - to - Noise Ratio Revealed

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# Introduction

- You may receive a **negative** FT8, JT65, or JT9 digital HF communications mode Signal-to-Noise Ratio (SNR) report in the range of -27 dB to -1dB
  - Recall , a negative SNR report implies the signal is below the noise floor
- **In reality, this is not the case, the Frequency Shift Key (FSK) tones are well above the noise floor**
- Received FT8, JT65 and JT9 signal reports are actually referenced to a **much wider noise bandwidth** (2500 Hz) than the actual **detection bandwidth** required to successfully decode the digital data represented by the received FSK tone.
- The smaller detection bandwidth drives the actual SNR, which along with forward-error-correction, allows error-free message decoding
- **The purpose of this presentation**
  - **To demonstrate the SNR increases dramatically as we home-in on the detection bandwidth of a single FSK tone**



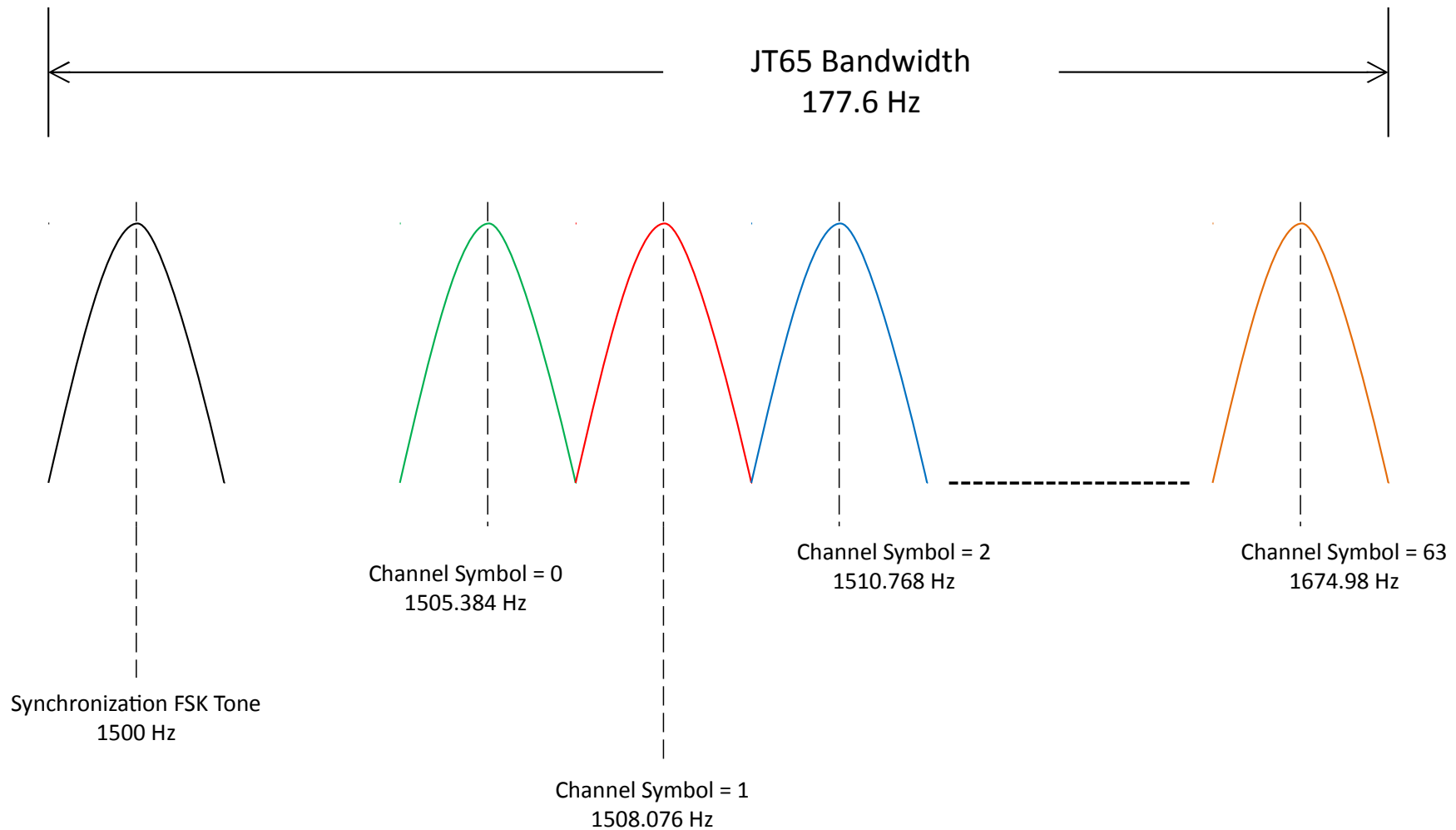
# What is Signal-to-Noise Ratio (S/N)

- **SNR is typically measured and reported in decibels (dB)**
- **S = received signal power as it is received by the distant end**
  - **It is the only variable** in this SNR equation **you can actually control**
- **How do you influence the received signal power at the distant end?**
  - Increasing/decreasing the transmit power
  - Using a higher gain antenna, etc.
  - You are in control of the Effective Radiated Power (ERP)
- **N = noise power as it is received by the distant end**
  - **Solely owned** by the operator on the distant end, the transmitting station has **no influence, whatsoever**, on the received noise power at the distant end
- **Noise comes from various sources:**
  - Atmospheric Noise (culmination of man-made noise and noise produced by lightning around the world)
  - Cosmic Noise (noise generated outside the earth's atmosphere)
  - Self-generated receiver noise



# What is the Detection Bandwidth, and the JT65 Waveform

*description bullets on next slide*





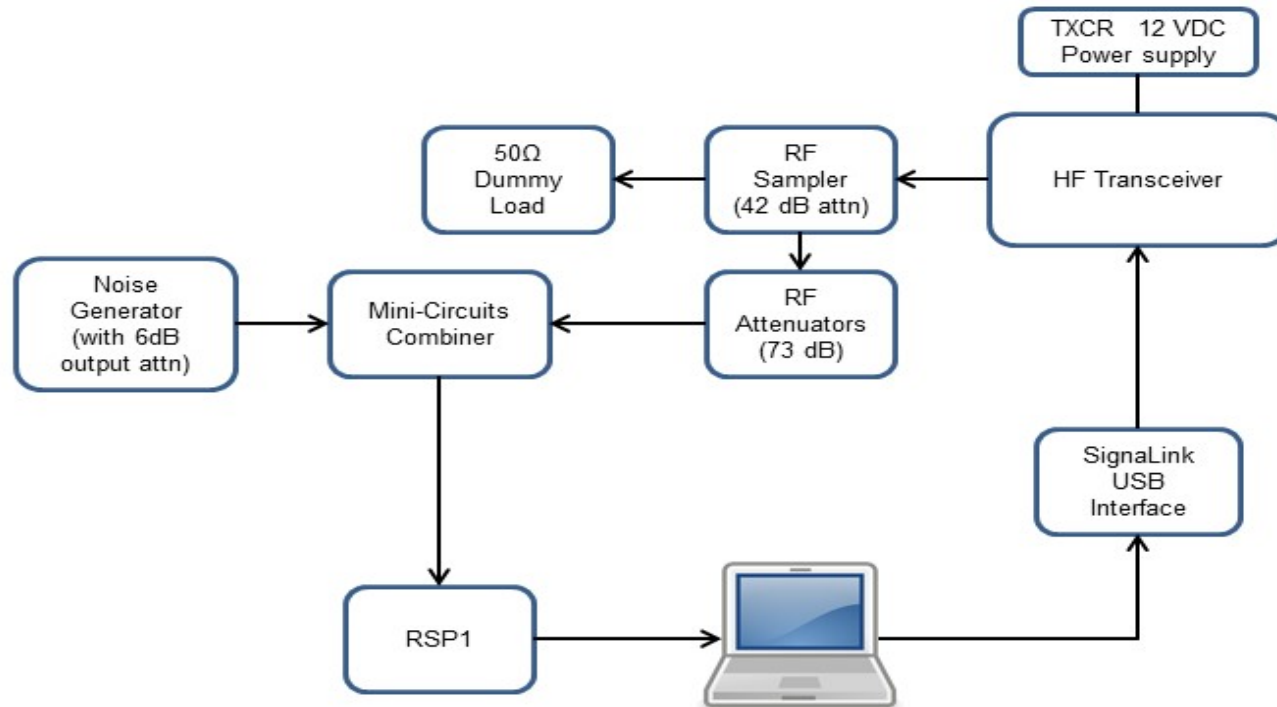
# The JT65 Waveform Description

- The JT65 waveform gets its name from the inventor Joe Taylor and the 65 refers to fact that it utilizes a **64-ary FSK tones waveform with one extra FSK tone maintaining time and frequency synchronization**
- Hence, **64 FSK tones, which carry the message data, plus 1 synchronization tone = 65**
- **The FSK sync tone is transmitted twice as frequently** as the FSK data tones during a message transmission
- Each of the 64 FSK tones represents a **6 bit encoded message symbol**
- The JT65 signaling waveform only occupies a **transmission bandwidth of approximately 178 Hz**
- **And even more significantly**, each FSK signaling tone, that is being transmitted only occupies **2.692 Hz – the detection bandwidth**
- **It is only the noise that exists in that super small bandwidth of 2.692 Hz** that drives the **real SNR** that determines the success of demodulating and decoding the text message
- The detection SNR is called the **FSK Symbol - to - Noise Power Density Ratio**



## The Test Configuration

*Used to demonstrate as we reduce the **Received Signal Report** referenced **2500 Hz Noise Bandwidth** to that which approaches the **very small Detection Bandwidth** the **SNR increases dramatically** (description on next slide)*





# Test Configuration Description

- **To demonstrate this, I put together a JT65 transmission and receiver system**
- The PC is running WSJT-X software to generate a **CQ KC5RUO DM65** message
- The **encoded message symbols** are sent via the SignalLink USB interface to the transceiver (YAESU FT-891) as FSK tones
- The FSK tones modulate a 20 meter 14.076 MHz carrier which is transmitted out and received by this SDRPlay Radio Spectrum Processor (RSP1) receiver **at a realistic signal power level that you might receive at home via your antenna system.**
- To get the signal down to a S1 S-unit level of approximately -121 dBm **I use a series of attenuators you see [here](#).** 115 dB of attenuation
- I am using the **SDRuno Software Defined Radio (SDR) signal processing software and receiver**, and in this *presentation* we are going to **focus on**:
  - The SP2, passband scope display
  - We'll be looking at the Signal Processing display and the waterfall
  - The RMS Power Level received power level measured in the SP2 defined bandwidth
    - Which is a measure of the signal and the noise within the SP2 defined bandwidth
  - The SNR, derived from the signal and noise power measured in the SP2 defined bandwidth
    - **Note: The SDRuno measured SNR is actually  $(S+N)/N$**
- To simulate received noise and set the received noise power, I use a Rigol DG4162 waveform function generator to produce the Additive White Gaussian Noise (AWGN)
- The Mini-circuits combiner brings both the signal generated by the transceiver and noise to the RSP1 receiver



SDRuno Screen Shot  
RSP1 Receiver Noise Floor  
SP2 passband = 2500 Hz

- Receiver Noise Bandwidth = 2500 Hz
- RSP1 Receiver Noise Floor  $\approx$  -130 dBm  
(9 dB below an S1 unit level)
- $N_{PB}$  = Noise Power derived from the SP2 passband
- $N_{PB} \approx$  -130dBm as measured across a receiver noise bandwidth = 2500 Hz



SDRuno MAIN

Final SR: 2000000  
IFBW: 1.536MHz (ZIF)  
Gain: 79.1dB

ADD VRX  
DEL VRX  
LO LOCK  
STOP  
MEM PAN

Sdr: 13%  
Sys: 14%

9/10/2018 2:38:56 PM Default Workspace

SDRuno RX CONTROL

STEP: 500 Hz  
14076000  
-130.0 dBm

MODE: AM SAM FM CW DSB LSB USB DIGITAL

VFO - QM FM MODE CW OP FILTER NB NOTCH

VFO A A > B NFM MFM CWPK 1800 2200 NBW NCH1

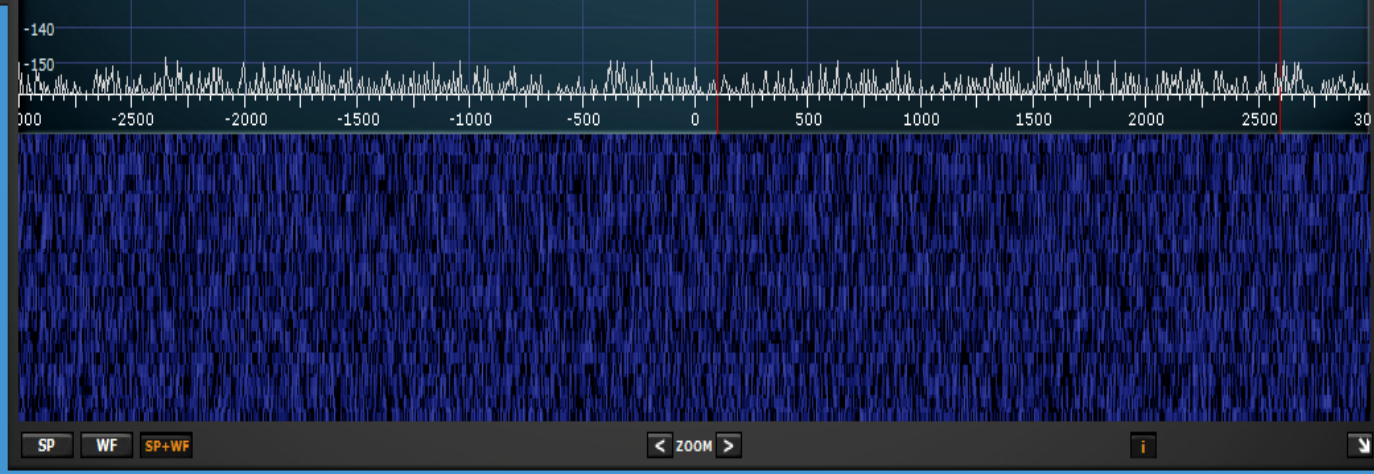
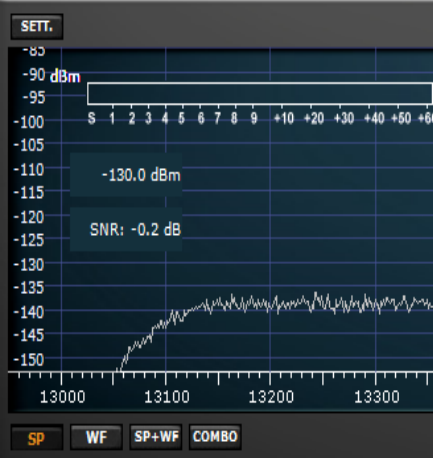
VFO B B > A WFM SWFM ZAP 2800 3000 NBN NCH2

QMS QMR CWAFNC NR NBOFF NCH3

-84 dB AGC OFF FAST NCH4

SQCL MUTE

0-00





# SDRuno Screen Shot

## JT65 Signal & RSP1 Receiver Noise Floor

### SP2 passband = 2500 Hz

- Receiver Noise Bandwidth = 2500 Hz
- $S_{PB}$  = Signal Power derived from the SP2 passband
- $S_{PB} \approx -121$  dBm = S1 unit level
- RSP1 Receiver Noise Floor  $N_{PB} \approx -130$ dBm **as measured across a receiver noise bandwidth = 2500 Hz**
- SNR  $\approx 9$  dB,
- Note:
  - SDRuno actual measured RMS power =  $(S_{PB} + N_{PB})$
  - And, SDRuno actual measured SNR =  $(S_{PB} + N_{PB}) / N_{PB}$
  - But, the JT65 signal level is so much larger than the Rx noise floor the measured RMS power and SNR are dominated by  $S_{PB}$

SDRuno MAIN

Final SR: 2000000  
IFBW: 1.536MHz (ZIF)  
Gain: 79.1dB

ADD VRX  
DEL VRX  
LO LOCK  
STOP  
MEM PAN

Sdr: 5%  
Sys: 31%

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SDRuno RX CONTROL

DEEMPH STEP: 500 Hz 14076000 -121.4 dBm RMS

MODE AM SAM FM CW DSB LSB USB DIGITAL

VFO - QM FM MODE CW OP FILTER NB NOTCH

VFO A A > B NFM MFM CWPK 1800 2200 NBW NCH1

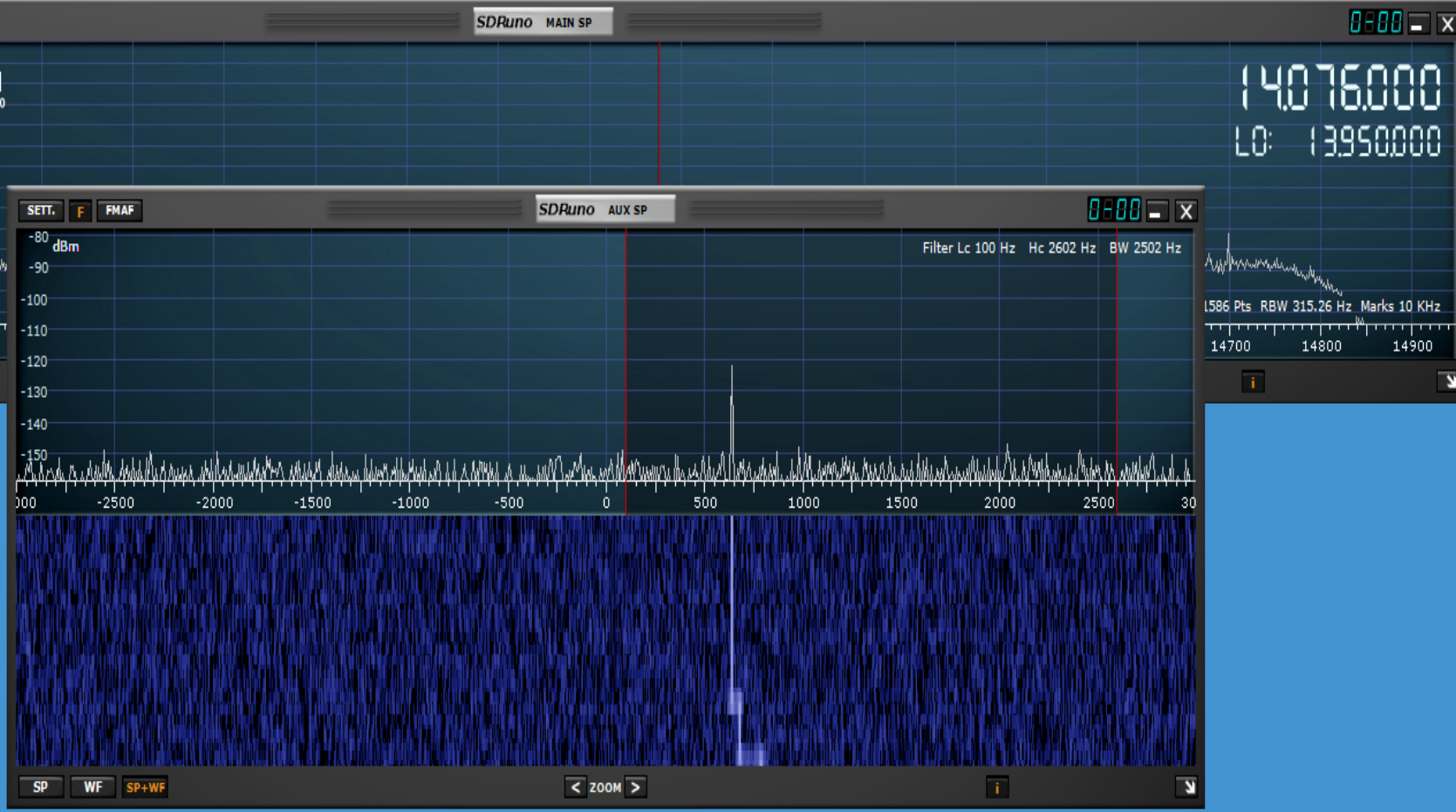
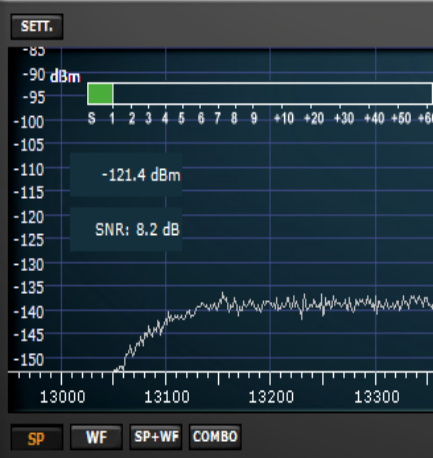
VFO B B > A WFM SWFM ZAP 2800 3000 NBN NCH2

QMS QMR CWAFK NR NBOFF NCH3

-84 dB AGC OFF FAST NCH4

SQCL MUTE

0-00





# SDRuno Screen Shot

## Received Additive White Gaussian Noise

- SP2 passband = 2500 Hz
- Receiver Noise Bandwidth = 2500 Hz
- AWGN power =  $N_{PB} \approx -115 \text{ dBm} = S2 \text{ unit level}$
- *As measured across a receiver noise bandwidth = 2500 Hz*

**SDRuno MAIN**

Final SR: 2000000  
IFBW: 1.536MHz (ZIF)  
Gain: 79.1dB

ADD VRX  
DEL VRX  
LO LOCK  
STOP  
MEM PAN

Sdr: 14%  
Sys: 16%

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**SDRuno RX CONTROL**

DEEMPH STEP: 500 Hz 14076000 -115.0 dBm RMS

MODE AM SAM FM CW DSB LSB USB DIGITAL

VFO - QM FM MODE CW OP FILTER NB NOTCH

VFO A A > B NFM MFM CWPK 1800 2200 NBW NCH1

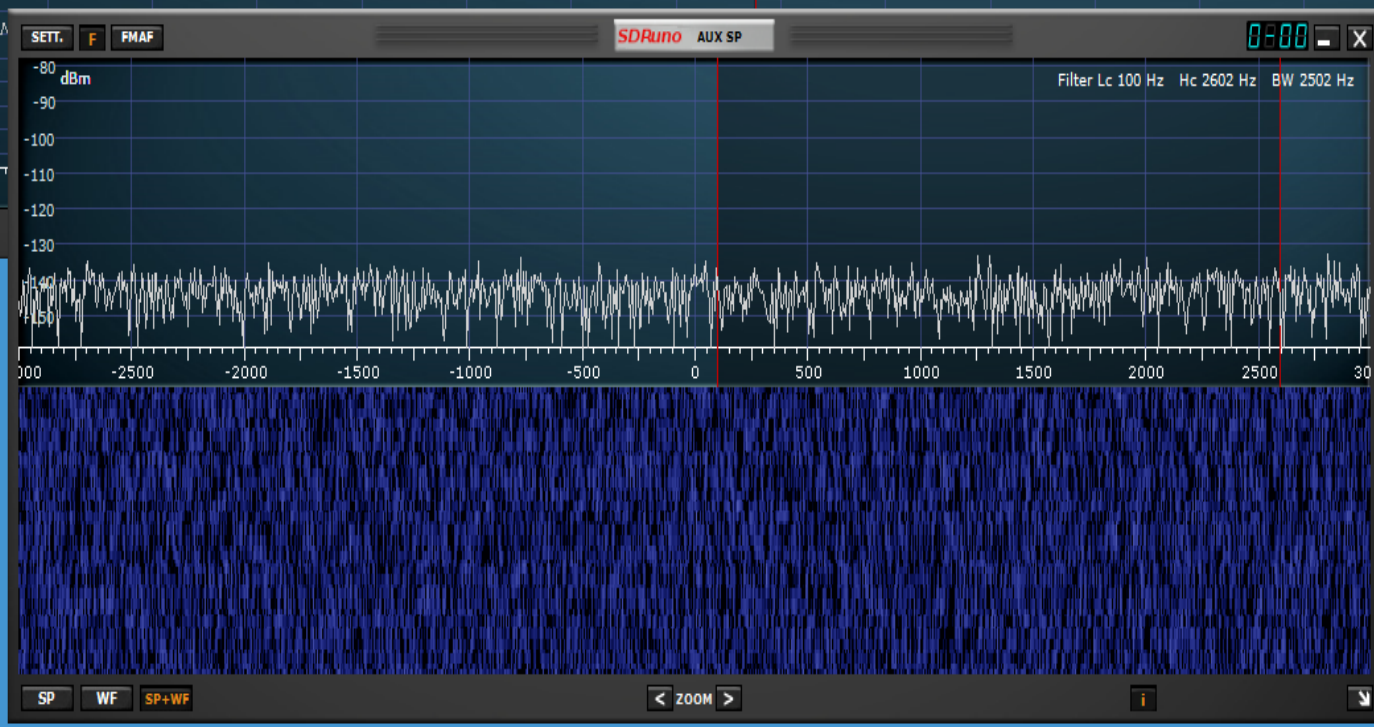
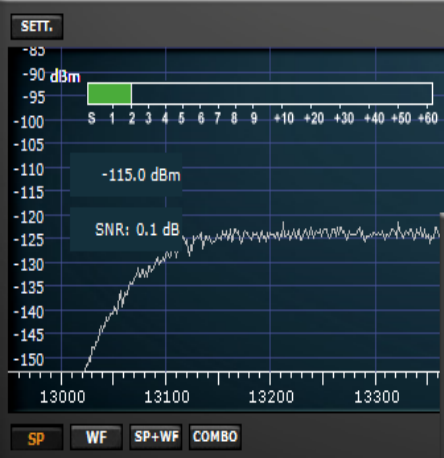
VFO B B > A WFM SWFM ZAP 2800 3000 NBN NCH2

QMS QMR CWAFC NR NBOFF NCH3

-84 dB AGC OFF FAST NCH4

SQCL MUTE

0-00





# SDRuno Screen Shot

## JT65 Signal & AWGN

### SP2 passband = 2500 Hz

- Receiver Noise Bandwidth = 2500 Hz
- $(S_{PB} + N_{PB}) = -114 \text{ dBm}$ 
  - Where  $S_{PB} = -121 \text{ dBm}$  and  $N_{PB} = -115 \text{ dBm}$
- $N_{PB} \approx 6 \text{ dB}$  greater than  $S_{PB}$  *as measured across a receiver noise bandwidth = 2500 Hz*
- The signal and noise power measurement **within the 2500 Hz** Receiver Noise Bandwidth is no longer dominated by the received JT65 signal but now dominated by the noise
- SNR measured value  $\approx 1.0 \text{ dB}$  ( $S_{PB} + N_{PB} = -114 \text{ dBm}$ ,  $N_{PB} = -115 \text{ dBm}$ )
  - Where  $\text{SNR} = (S_{PB} + N_{PB}) / N_{PB}$ , and dominated by  $N_{PB}$  *as measured across a receiver noise bandwidth = 2500 Hz*

SDRuno MAIN

Final SR: 2000000  
IFBW: 1.536MHz (ZIF)  
Gain: 79.1dB

ADD VRX  
DEL VRX  
LO LOCK  
STOP  
MEM PAN

Sdr: 7%  
Sys: 36%

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SDRuno RX CONTROL

STEP: 14076000 -114.3 dBm RMS

500 Hz

MODE: AM SAM FM CW DSB LSB USB DIGITAL

VFO - QM FM MODE CW OP FILTER NB NOTCH

VFO A A > B NFM MFM CWPK 1800 2200 NBW NCH1

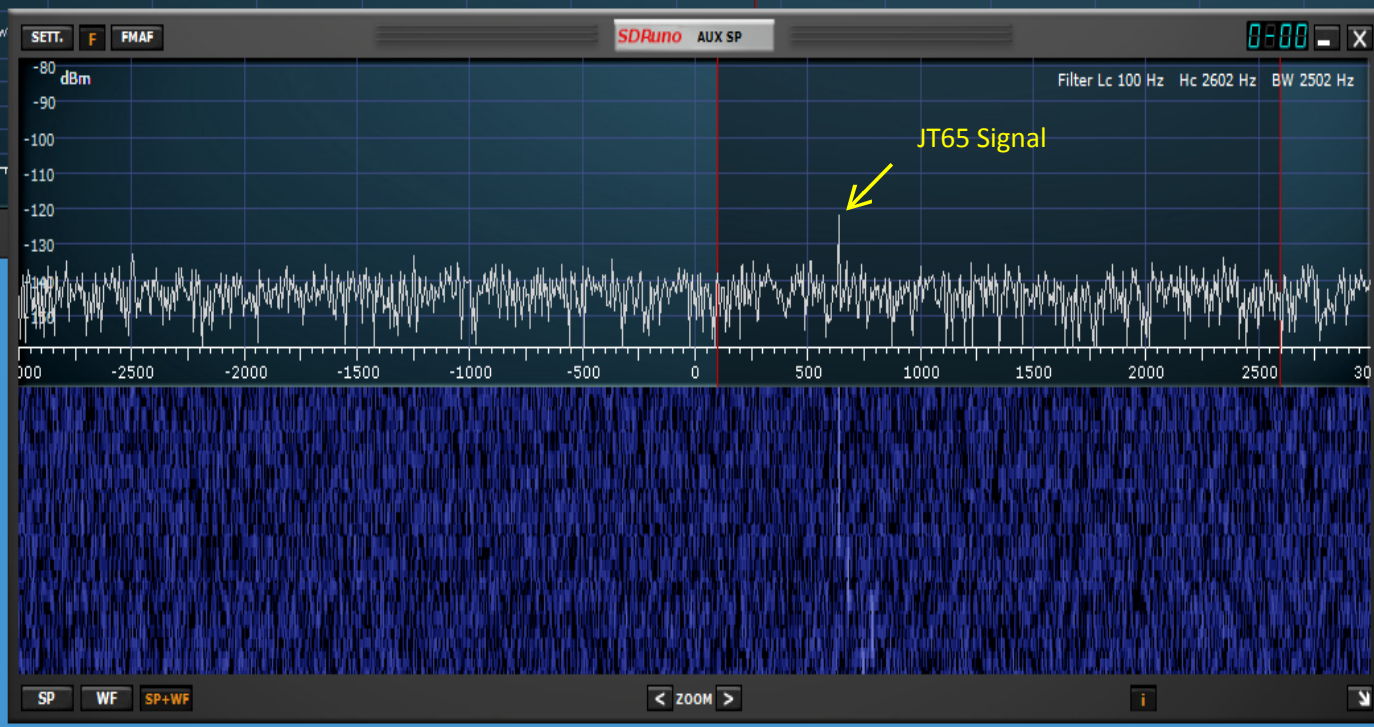
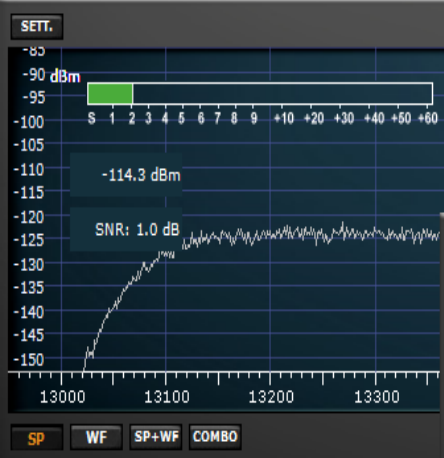
VFO B B > A WFM SWFM ZAP 2800 3000 NBN NCH2

QMS QMR CWAFK NR NBOFF NCH3

-84 dB AGC OFF FAST NCH4

SQCL MUTE

0-00





# SDRuno Screen Shot JT65 Signal & AWGN

Receiver Noise Bandwidth = 2500 Hz

- **So why can we still see the FSK tones rise above the noise floor?**
- Because the FSK signal energy is concentrated over a very small bandwidth of 2.692 Hz. The FSK tone detection BW = 2.692 Hz
- The signal energy in that small concentrated BW is much greater than the noise power over that detection bandwidth.
- You see, **if the FSK tone bandwidth was actually 2500 Hz** we would never see the signal. The signal energy would be spread out over the 2500 Hz receiver noise bandwidth and “buried in the weeds”.
- **It is the SNR within that FSK tone detection BW which determines the success or failure of demodulating and decoding an error-free JT65 message - not the reported SNR referenced across the much wider 2500 Hz noise bandwidth**





## The Claim

As the receiver noise bandwidth decreases and approaches that of the actual detection bandwidth the SNR increases.

- I am going to change the SP2 receiver passband to 179 Hz the approximate transmission bandwidth of the JT65 signal
- Recall the JT65 transmission bandwidth encompasses the FSK sync tone and the 64 FSK message tones



# SDRuno Screen Shot JT65 Signal & AWGN SP2 passband = 179 Hz

- Receiver Noise Bandwidth = 179 Hz
- $N_{PB}$  is significantly reduced
- $(S_{PB} + N_{PB}) = -121$  dBm
  - Where  $S_{PB} = -121$  dBm and  $N_{PB} = -127$  dBm
- The signal and noise power measurement **within the 179 Hz** Receiver Noise Bandwidth is again dominated by the received JT65 signal
- SNR measured value  $\approx 6$  dB
  - SNR increased approx 5 dB, a factor of 3 times higher SNR

SDRuno MAIN

Final SR: 2000000  
IFBW: 1.536MHz (ZIF)  
Gain: 79.1dB

ADD VRX  
DEL VRX  
LO LOCK  
STOP  
MEM PAN

Sdr: 8%  
Sys: 10%

9/10/2018 3:22:45 PM Default Workspace

SDRuno RX CONTROL

DEEMPH STEP: 500 Hz 14076000 -121.1 dBm RMS

MODE AM SAM FM CW DSB LSB USB DIGITAL

VFO - QM FM MODE CW OP FILTER NB NOTCH

VFO A A > B NFM MFM CWPK 1800 2200 NBW NCH1

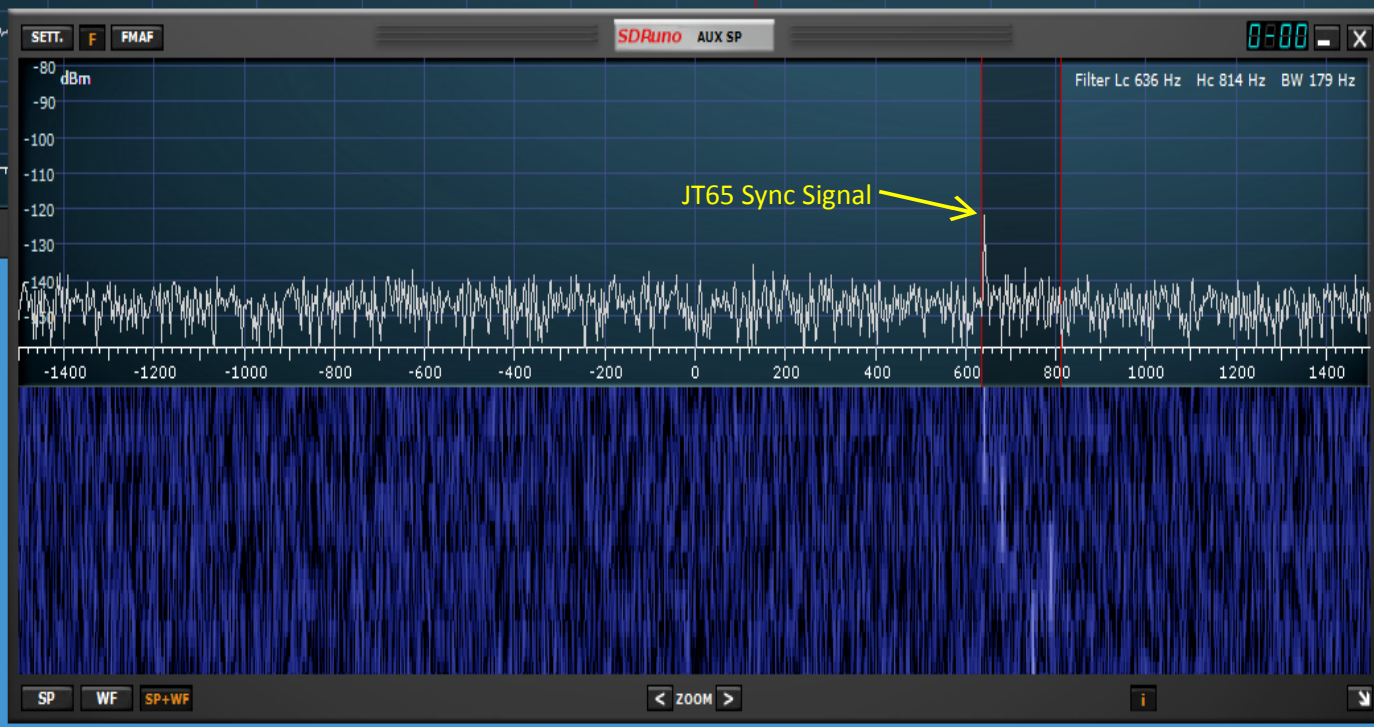
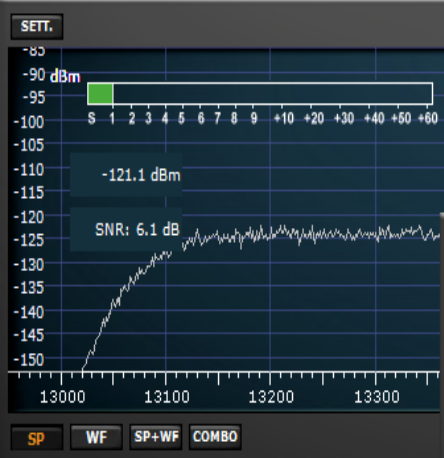
VFO B B > A WFM SWFM ZAP 2800 3000 NBN NCH2

QMS QMR CWAFK NR NBOFF NCH3

-84 dB AGC OFF FAST NCH4

SQCL MUTE

0-00





## Close In on the Detection Bandwidth Receiver Noise Bandwidth = 9 Hz

- Now I am going to close in on the JT65 FSK sync tone and try to get as close to the detection bandwidth as possible
  - By reducing the receiver passband to something as close to that which approaches the 2.692 Hz detection bandwidth



# SDRuno Screen Shot JT65 Signal & AWGN SP2 passband = 9 Hz

- Receiver Noise Bandwidth = 9 Hz
- $N_{PB}$  is further significantly reduced
- $(S_{PB} + N_{PB}) = -121$  dBm
  - Where  $S_{PB} = -121$  dBm and  $N_{PB} = -138$  dBm
- The signal and noise power measurement **within the 9 Hz** Receiver Noise Bandwidth is again dominated by the received JT65 signal
- SNR measured value  $\approx 17$  dB
  - SNR increased by a factor of 40

**SDRuno MAIN**

Final SR: 2000000  
IFBW: 1.536MHz (ZIF)  
Gain: 79.1dB

ADD VRX  
DEL VRX  
LO LOCK  
STOP  
MEM PAN

Sdr: 10%  
Sys: 11%

9/10/2018 3:35:31 PM Default Workspace

**SDRuno RX CONTROL**

STEP: 14076000 -123.4 dBm RMS

DEEMPH 500 Hz

MODE AM SAM FM CW DSB LSB USB DIGITAL

VFO - QM FM MODE CW OP FILTER NB NOTCH

VFO A A > B NFM MFM CWPK 1800 2200 NBW NCH1

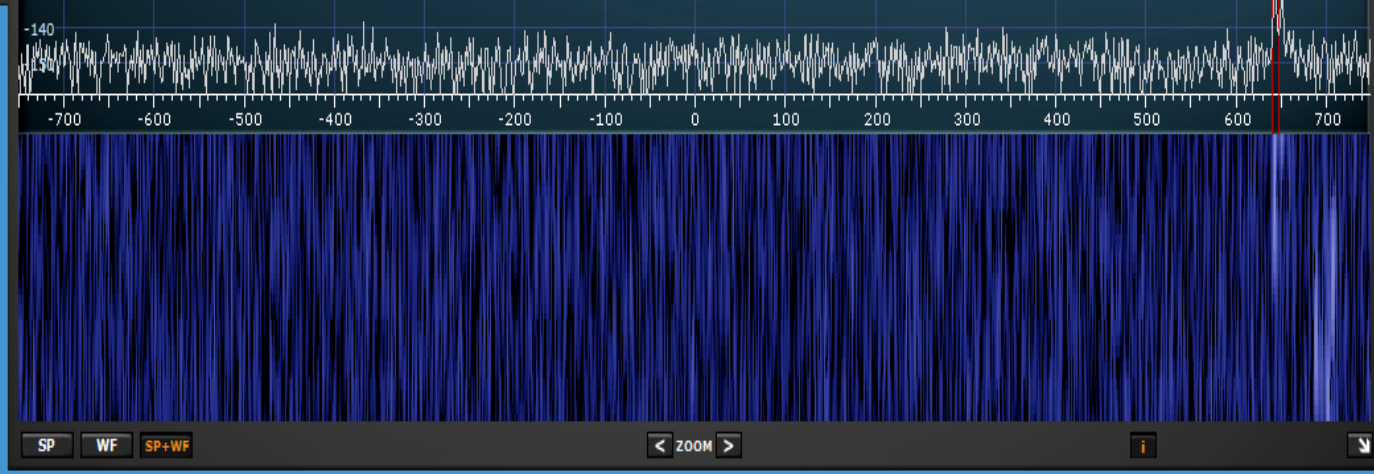
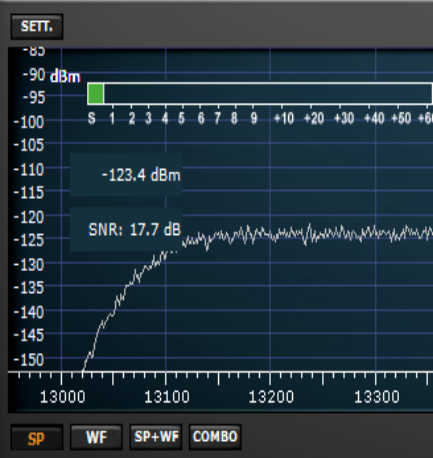
VFO B B > A WFM SWFM ZAP 2800 3000 NBN NCH2

QMS QMR CWAFC NR NBOFF NCH3

-84 dB AGC OFF FAST NCH4

SQCL MUTE

0-00





## So, what is the Real SNR that determines JT65, JT9, FT8 Message Decoding Performance?

- FSK Symbol – to – Noise Power Density Ratio ( $E_s/N_o$ )
- $(E_s/N_o)_{dB}$  can be derived mathematically from the **Reported SNR**

$$(E_s/N_o)_{dB} = (SNR_{reported})_{dB} + (10 \times \text{LOG} (2500 \text{ Hz} / (\text{FSK symbol detection BW}))_{dB}$$

- JT65 FSK symbol detection BW = 2.692 Hz
- JT9 FSK symbol detection BW = 1.736 Hz
- FT8 FSK symbol detection BW = 6.25 Hz



# HF Digital Communication Mode JT65

$$(Es/No)_{JT65 (dB)} = (SNR_{reported})_{JT65 (dB)} + (10 \times \text{LOG} (2500 \text{ Hz}/2.692 \text{ Hz}))_{(dB)}$$

where:

- 1) 2500 Hz is the Reported SNR Noise bandwidth
- 2) 2.692 Hz is the actual JT65 signaling noise bandwidth also known as the JT65 FSK symbol detection bandwidth

$$(Es/No)_{JT65 (dB)} = (SNR_{reported})_{JT65 (dB)} + 29.7 \text{ dB}$$





# HF Digital Communication Mode JT9

$$(Es/No)_{JT9 (dB)} = (SNR_{reported})_{JT9 (dB)} + (10 \times \text{LOG} (2500 \text{ Hz}/1.736 \text{ Hz}))_{(dB)}$$

where:

- 1) 2500 Hz is the Reported SNR Noise bandwidth
- 2) 1.736 Hz is the actual JT9 signaling noise bandwidth also known as the JT9 FSK symbol detection bandwidth

$$(Es/No)_{JT9 (dB)} = (SNR_{reported})_{JT9 (dB)} + 31.6 \text{ dB}$$



# HF Digital Communication Mode FT8

$$(Es/No)_{FT8 (dB)} = (SNR_{reported})_{FT8 (dB)} + (10 \times \text{LOG} (2500 \text{ Hz}/6.25 \text{ Hz}))_{(dB)}$$

where:

- 1) 2500 Hz is the Reported SNR Noise bandwidth
- 2) 6.25 Hz is the actual FT8 signaling noise bandwidth also known as the FT8 FSK symbol detection bandwidth

$$(Es/No)_{FT8 (dB)} = (SNR_{reported})_{FT8 (dB)} + 26 \text{ dB}$$



JT65, JT9, and FT8 FSK Symbol-to-Noise Density Ratio $(E_s/N_0)_{dB}$ derived from Reported SNR			
Reported SNR (dB) over a 2500 Hz Noise Bandwidth	$(E_s/N_0)_{JT65}$ (dB)	$(E_s/N_0)_{JT9}$ (dB)	$(E_s/N_0)_{FT8}$ (dB)
-30	-0.3	1.6	-4
-29	0.7	2.6	-3
-28	1.7	3.6	-2
-27	2.7	4.6	-1
-26	3.7	5.6	0
-25	4.7	6.6	1
-24	5.7	7.6	2
-23	6.7	8.6	3
-22	7.7	9.6	4
-21	8.7	10.6	5
-20	9.7	11.6	6
-19	10.7	12.6	7
-18	11.7	13.6	8
-17	12.7	14.6	9

SNR threshold referenced to a 2500 Hz BW at a 50% probability for decoding a JT9 message in AWGN

SNR threshold referenced to a 2500 Hz BW at a 50% probability for decoding a JT65 message in AWGN

SNR threshold referenced to a 2500 Hz BW at a 50% probability for decoding a FT8 message in AWGN



# Takeaways

- JT65, JT9 and FT8 SNR reports are referenced to a much wider noise bandwidth, 2500 Hz, than is required to successfully demodulate and decode the message
- The SNR associated with the FSK tone detection BW or signaling bandwidth is the real SNR and it is much larger than the reported SNR
- Our amateur radio receiver's ability to successfully demodulate/decode the signal of interest is all dependent upon the noise level that exists over the detection bandwidth – whether it is CW, Phone, BPSK31, etc.
- 
- **So why are the received signal reports based upon a 2500 Hz bandwidth?**
  - SNR is reported for all amateur radio modes traditionally based on a receiver bandwidth of 2500 Hz
  - Because JT65, JT9 and FT8 digital HF communication modes are usually received with a normal SSB receiver, whose **IF filter is approximately 2500 Hz wide**



# References

1. ***Work the World with WSJT-X, Part 2: Codes, Modes, and Cooperative Software Development***, Joe Taylor, K1JT; Steve Frankie, K9AN, and Bill Somerville, G4WJS, ARRL QST, November 2017, Volume 101, Number 11.
2. ***Open Source Soft-Decision Decoder for the JT65 (63,12) Reed-Solomon Code***, Steven J. Frankie, K9AN and Joseph H. Taylor, K1JT, QEX, May/June 2016.
3. ***Work the World with JT65 and JT9, Digital Communication via Amateur Radio***, Steve Ford, WB8IMY, ***JT65 and JT9 Protocol Specifics***, by Dr Joe Taylor, K1JT, pg 1-6, ARRL Inc, ISBN: 978-1-62595-043-7



# Handout

- You are welcome to the handout which shows the real SNR for a given Reported SNR
- The real SNR is provided for JT65, JT9 , and FT8
- The other side of the handout shows the algorithm used to derive the real SNR